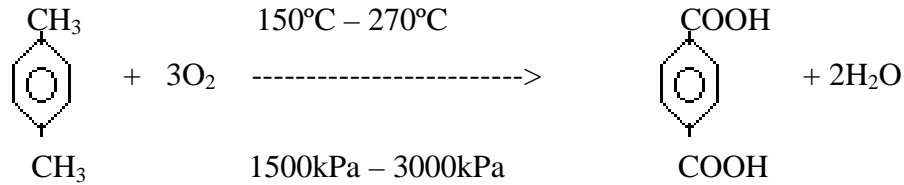


# MATERIAL BALANCE

## CHEMICAL REACTION:



## OVERALL BALANCE:

Basis:  $750 \times 10^3$  Kg of Terephthalic acid

Given:

Purity of Product - 99%

Conversion - 95%

Solvent - 0.05 Kg / Kg of product

O<sub>2</sub> - 5 – 15 % excess from theoretical value

### **For 1 day basis:**

#### **Product:**

From data product is 99% pure assume rest 1% is water.

Therefore amount of product (Terephthalic acid) = 742500 Kg = 4472.89 Kmoles

Water associated with it = 7500 Kg = 416.67 Kmoles

#### **Feed:**

From the chemical equation 1 Kmole of p-Xylene = 1 Kmole of Product

But given that conversion is 95%

Therefore 1 Kg mole of p- xylene = 0.95 of Terephthalic acid

Therefore amount of p-Xylene reqd. =  $4472.89/0.95 = 4708.31$  Kmoles = 499080.86 Kg

Unconverted Feed =  $0.05 \times 4708.31 = 235.41$  Kmoles = 24953.46 Kg

#### **Air:**

1 Kmole of p-Xylene = 3 Kmoles of Oxygen

Therefore theoretical amount of Oxygen reqd. =  $4708.31 \times 3 = 14124.92$  Kmoles

An excess of 15 % is used to inhibit the formation of byproducts

Excess amount of oxygen =  $14124.92 \times 0.15 = 2118.74$  Kmoles

Total amount of Oxygen = 16243.66 Kmoles

Nitrogen associated =  $(79/21) \times 16243.66 = 61107.1$  Kmoles

Total Air required = 77350.76 Kmoles =  $2229.79 \times 10^3$  Kg

**Water:**

1 Kmole of PTA = 2 Kmole of H<sub>2</sub>O

Amount of water formed =  $4472.89 \times 2 = 8945.78$  Kmoles =  $161.02 \times 10^3$  Kg

**Oxygen in outlet:**

Amount of oxygen leaving the system = 5% unreacted + 15% excess

Amount of oxygen leaving = 2824.99 Kmoles =  $90.399 \times 10^3$  Kg

**Solvent Required:**

Given that solvent required = 0.05 Kg/Kg of PTA

Amount of Acetic Acid required = 625 Kmoles =  $37.5 \times 10^3$  Kg

**Balance across each equipment:**

Reactor & G-L separator:

Basis : 1 Day operation

**INLET:**

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	4708.31	499.01
Acetic Acid	625	37.5
Air	77350.76	2229.79

Total :  $2766.3 \times 10^3$  Kg

**OUTLET:**

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	235.41	24.95
Acetic Acid	625	37.5
Water Formed	8945.78	161.02
Air	63932.09	1800.39
Terephthalic acid	4472.89	742.5

Total:  $2766.3 \times 10^3$  Kg

**Surge Tank:**

**INLET:**

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	235.41	24.95
Acetic Acid	625	37.5
Water Formed	8945.78	161.02
Air	63932.09	1800.39
Terephthalic acid	4472.89	742.5

Total: 2766.3 x 10<sup>3</sup> Kg

**OUTLET:**

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	235.41	24.95
Acetic Acid	625	37.5
Water Formed	8945.78	161.02
Air	63932.09	1800.39
Terephthalic acid	4472.89	742.5

Total: 2766.3 x 10<sup>3</sup> Kg

**Centrifuge:**

**INLET:**

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	235.41	24.95
Acetic Acid	625	37.5
Water Formed	8945.78	161.02
Air	63932.09	1800.39
Terephthalic acid	4472.89	742.5

Total: 2766.3 x 10<sup>3</sup> Kg

In the centrifuge two streams separate out

- i. Stream to the Rotary Drier (solid + moisture)
- ii. Stream to the Residue Still

*To Estimate the amount of water entering the Drier:*

Assume the drier is capable of removing 60% moisture entering.

We have outlet from the drier as

Terephthalic acid solid = 4472.89 Kmoles.

Water associated with it = 416.67 Kmoles.

Let  $y$  be the amount of water in inlet of the drier.

$y - 0.6 y = 416.67$  Kmoles.

Therefore the inlet to the drier  $y = 416.67/0.4 = 1041.68$  Kmoles =  $18.75 \times 10^3$  Kgs.

Water removed in the drier (60%) =  $11.25 \times 10^3$  Kgs.

Water to the residue still =  $142.3 \times 10^3$  Kgs.

***Drier:***

***INTLET:***

Acetic acid enters the drier in a negligible amount and hence can be neglected

Component	Kmoles	Kg x 10 <sup>-3</sup>
Water	1041.67	18.75
Terephthalic acid	4472.89	742.5

Total:  $761.25 \times 10^3$  Kg

***OUTLET:***

Component	Kmoles	Kg x 10 <sup>-3</sup>
Water	416.67	7.5
Terephthalic acid	4472.89	742.5

Water Lost (evaporated) :  $11.25 \times 10^3$  Kgs

Total :  $761.25 \times 10^3$  Kgs

***Residue Still:***

***INLET:***

Component	Kmoles	Kg x 10 <sup>-3</sup>
p-Xylene	235.41	24.95
Acetic Acid	625	37.5
Water Formed	7905.56	142.3

Total :  $204.75 \times 10^3$  Kgs

**OUTLET:**

p-Xylene is a heavy key and hence in trace amounts in the distillate.

From the data it is given that about 80 – 95 % of acetic acid is recovered hence assume that 20%(mole) goes in the residue stream and about 10%(mole) of water entering goes in the residue.

Component	Distillate (Kgs) x 10 <sup>3</sup>	Residue (Kg) x 10 <sup>3</sup>
p-Xylene	-	24.95
Acetic Acid	35.68	1.82
Water Formed	128	14.3

Total : 204.75 x 10<sup>3</sup> Kgs

**Condenser:**

Considering the reflux for the still reflux is taken as 0.6

The vapor entering the condenser = 1.6 x 163.68 x 10<sup>3</sup> Kgs = 261.89 x 10<sup>3</sup> Kgs.

Reflux to the Still = 98.21 x 10<sup>3</sup> Kgs.

Feed to the dehydration tower = 163.68 x 10<sup>3</sup> Kgs.

**Dehydration Tower:**

**INLET:**

Acetic Acid : 24.738 Kmole/Hr

Water : 296.25 Kmoles/Hr

Feed : 321 Kmoles/Hr

$X_F = 0.93$

$F X_F = D X_D + W X_W$

W (Residue) = 22.134 Kmoles/Hr

D (Distillate) = 298.866 Kmoles/Hr

$X_D = 0.998, X_W = 0.012$

Assume reflux ratio is 0.6

**Condenser:**

Feed to the condenser = 1.6 x 5.379 x 10<sup>3</sup> Kgs/Hr = 8.61 x 10<sup>3</sup> Kgs/Hr

Reflux to the dehydration tower = 3.23 x 10<sup>3</sup> Kgs/Hr

Distillate (water) = 5.379 x 10<sup>3</sup> Kg/Hr