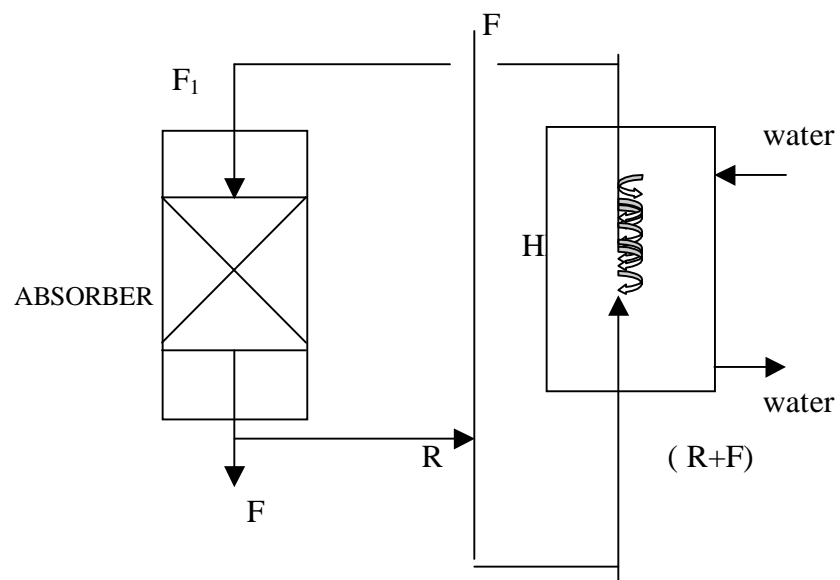


## 6. HEAT BALANCE

### 1. SHELL AND TUBE HEAT EXCHANGER

Since all the reactions in absorber and even formation of aq.ammonia, which is sent to absorber are exothermic reaction the heat of reaction should be removed off from absorber section, to maintain it at a low temperature of 20<sup>0</sup>c. This task is achieved by installing a shell and tube heat exchanger to the stream that is being sent to the absorber section a part of bottoms of absorber is recycled to achieve the good conversion.

### Determination of temperature of inlet and outlet stream to the heat exchanger.



Basis: 1 hour operation.

Let  $(\text{NH}_4\text{OH})$  stream from tank =  $F$  kg

Let  $R$  kg be recycle stream to HE

Assuming  $R$  be 50% of  $F_1$

$$\therefore R = 0.50 [ R + F ]$$

$$0.5R = 0.5F$$

$$(\therefore F_1 = R + F)$$

$$\therefore \boxed{\phantom{0.74}}$$

Hence, recycle  $R = F = 7176.5 \text{ kg}$

Let 'X' be mass fraction of  $\text{NH}_4\text{OH}$  in recycle stream to HE (2) consider 15% conversion in absorption tower.

$$X = \frac{(F + RX) \times (1 - 0.15)}{F + R}$$

$$X = \frac{(1+X) \times 0.85}{2}$$

$$X = 1 / 1.35 = 0.74$$

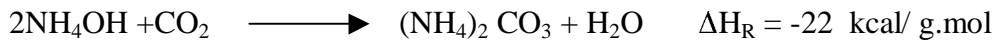
$$\boxed{X = 0.74}$$

The total mass of stream fed back to the absorber tower,

$$\begin{aligned} F_1 &= \frac{R \cdot X}{35} + \frac{(1 - X)F}{96} \\ &= \frac{(FX + F)}{35} + \frac{(1 - X)F}{96} \\ &= F \frac{(1 + X)}{35} + \frac{F(1 - X)}{96} \\ &= \frac{7176.5(1+0.74)}{35} + \frac{7176.5(1 - 0.74)}{96} \\ &= \underline{376.2 \times 10^3 \text{ g mol}} = 14353 \text{ kg/hr} \end{aligned}$$

Stream sent to the heat exchanger is  $376.2 \times 10^3$  g mol or 14353 kg/hr. In reality it is a mixture of Aq. Ammonia and ammonium carbonate but concentration of ammonium carbonate is too small that the entire stream can be considered as containing only Aq. Ammonia.

### Heat liberated



$$\begin{aligned} \text{In terms of NH}_4\text{OH} \quad \Delta H_R &= 22/2 \\ &= 11 \text{ Kcal/gmol of NH}_4\text{OH} \end{aligned}$$

$$\begin{aligned} \therefore \text{Total heat liberated } Q &= F_1 \times \Delta H_R \times 0.15 \\ Q &= 376.2 \times 10^3 \times 11 \times 10^3 \times 0.15 \\ Q &= 0.620 \times 10^9 \text{ cal} \\ \text{Or } Q &= 2.60 \times 10^9 \text{ J} \end{aligned}$$

This amount of Q is to be recovered in heat exchanger

$$\therefore Q = F_1 \times C_p \times (T - T_r)$$

$$\underline{T_r = 20^\circ\text{C}}$$

$$C_p \text{ of NH}_4\text{OH} = 90 \text{ J/g.mol}^\circ\text{C}$$

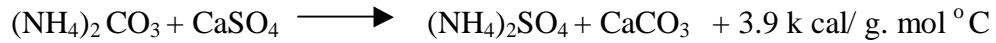
$$\therefore 2.60 \times 10^9 = 376.1 \times 10^3 \times 90 [T - 20]$$

$$\therefore T = 96.81 \approx 97^\circ\text{C}$$

$$\text{or } T = 97^\circ\text{C}$$

## 2. REACTOR SECTION

The reaction taking place in the reactor is,



96 % of conversion is assumed. The reaction is exothermic, but reactor temperature has to be maintained at room temperature. The heat produced is removed by installing cooling coils in the reactor.

Heat generated in the reactor  $Q = F \times \Delta H_R \times \% \text{ conversion}$ .

$$= 9842/96 \times 3.9 \times 10^3 \times 0.96$$

$$= 383.84 \text{ KJ}$$

the outlet stream contains ammonium sulphate, ammonium carbonate and calcium carbonate.

### In the exit stream

$$\text{Amount of ammonium sulphate} = 10517/132 = 79.67 \text{ g.mol}$$

$$\text{Amount of calcium carbonate} = 9700/100 = 97 \text{ g.mol}$$

$$\text{Amount of ammonium carbonate} = 843.5/96 = 8.78 \text{ g. mol}$$

$$\text{Specific value of ammonium sulphate} = 1.63 \text{ KJ / Kg } ^\circ\text{C} = 215.1 \text{ J / g.mol}$$

$$\text{Specific value of calcium carbonate} = 1.20 \text{ KJ / Kg } ^\circ\text{C} = 120.5 \text{ J / g.mol}$$

$$\text{Specific value of ammonium carbonate} = 3.10 \text{ KJ / Kg } ^\circ\text{C} = 298.5 \text{ J / g.mol}$$

### Rise in temperature

The total heat in the reactor exit stream Q,

$$Q = 383.84 \times 10^3 = [79.69 \times 215.1 + 97 \times 120.5 + 8.78 \times 298] \times (T - 30)$$

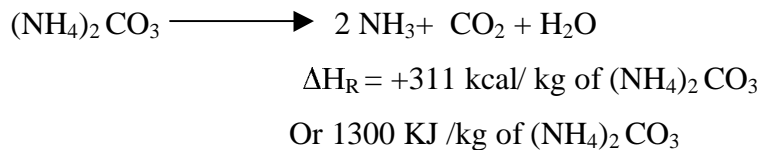
$$\therefore T = 42 \text{ }^\circ\text{C}$$

Hence cooling water requirement =  $m = (383.84 \times 10^3) / (4.184 \times (42 - 30))$

$$= \underline{1.835 \text{ kg/hour}}$$

### DECOMPOSER SECTION.

In decomposer, the un-reacted ammonium carbonate from reactor outlet stream will be decomposed off into ammonia, carbon dioxide and water. The decomposition reaction is:



The reaction is endothermic in nature i.e. the decomposition of ammonium carbonate requires heat of decomposition. This can be achieved by supplying steam into through stem coil inside the decomposer. this decomposition of ammonium carbonate is achieved above 109°C.

Heat required by decomposer Q<sub>d</sub>:

$$Q_d = \begin{array}{l} \text{heat require} \\ \text{stream to decomposition} \\ \text{temperature} \end{array} + \begin{array}{l} \text{heat required for decomposition} \\ \text{reaction} \end{array}$$

$$Q_d = (m_{as} c_{p1} + m_{water} c_{p2} + m_{ac} c_p) (109 - 30)$$

$$Q_d = [ 109417 \times 1.63 + 657.7 \times 4.184 + 843.5 \times 3.10 ] (109 - 30) = 843.5 \times 1300$$

$$Q_d = 2861 \text{ KJ}$$

Steam requirement.

It is assumed that saturated steam is supplied and the exhaust stream would be of saturated liquid

Amount of steam required for decomposition of ammonium carbonate,  $m_h$

$$m_h = 2861 / 1.80 (100 - 0) = \underline{15.69 \text{ kg / hour}}$$

#### 4. KRYSTAL EVAPORATOR.

In this section evaporative crystallisation takes place.

Amount of water to be evaporated = 345 kg.

Assuming the steam side is at higher pressure, i.e. 2 atmospheres.

Amount of heat required for evaporation =  $m \lambda_1$

$$= 345 \times 2256.9 \quad (\lambda_1 = 2256.9 \text{ KJ/ kg})$$

$$= \mathbf{778.63 \times 10^3 \text{ KJ/ kg}}$$

At 2 atmospheric pressure latent heat of steam  $\lambda_2 = 2198.18 \text{ KJ/ kg}$

$$\text{Amount of steam required} = 778.63 \times 10^3 / (2198.18)$$

$$= \mathbf{354.18 \text{ kg / Hr}}$$